# Interfacial Characterization and Minimum Miscible Pressure Study of CO<sub>2</sub> Flooding Based on Molecular Dynamics

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#### **Abstract**

CO<sup>2</sup> flooding can not only effectively improve the recovery of oil reservoirs, but also permanently store  $CO<sub>2</sub>$  underground to alleviate the greenhouse effect. In the process of  $CO<sub>2</sub>$  flooding,  $CO<sub>2</sub>$  is injected into the oil reservoirs to affect the properties of crude oil through adsorption on oil interface, which reduces the interfacial tension and the density of the crude oil, thereby enhancing the recovery factor. Conventional core flooding experiments can only observe the oil displacement effect from a macroscopic perspective, but it is difficult to characterize the interface of  $CO<sub>2</sub>$  flooding from a microscopic perspective. Furthermore, the experiment to obtain the minimum miscible pressure (MMP) usually requires a long time and high cost.

In this study, an all-atom molecular dynamics simulation method was used to establish a  $CO<sub>2</sub>$  model and a crude oil model. Using the  $CO<sub>2</sub>$  force field of ZHU and the alkane force field of NERD, the interface interaction, interface characteristics, and minimum miscible pressure between  $CO<sub>2</sub>$  and crude oil were analyzed. The research results show that when  $CO_2$  mixes with the crude oil,  $CO_2$  accumulates at the interface to form an adsorption layer; with the increase of system pressure, the phase interface and the  $CO<sub>2</sub>$  adsorption layer gradually become thicken, and the interfacial tension (IFT) between  $CO<sub>2</sub>$  and crude oil decreases linearly. The addition of the light hydrocarbon component allows  $CO<sub>2</sub>$  to be more readily miscible with crude oil. At a low pressure, IFT decreases with increasing temperature, while at a high pressure, IFT increases with increasing temperature and MMP increases with increasing temperature as well. The MMP calculated using linear extrapolation of the interfacial tension was in good agreement with the experiment measurements.

The main innovations of this study was the use of molecular dynamics analysis to simulate the interfacial properties of a system composed of  $CO<sub>2</sub>$  and n-alkanes, and it is applicable to apply the simulated MMP in real oilfields. This study can significantly reduce the human, material and financial resources of the experiment in estimating MMP and also provide constructive suggestions on the practical application of CO<sup>2</sup> flooding on oil reservoirs.

#### **Introduction**

In domestic and international reservoir development,  $CO<sub>2</sub>$  flooding can not only enhance oil recovery, but also achieve  $CO<sub>2</sub>$  sequestration and reduce the greenhouse effect. When the pressure is high enough, the ability of the crude oil to dissolve bitumen and paraffin decreases after  $CO<sub>2</sub>$  precipitates the lighter

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components in the crude oil, and the heavy components precipitate out of the crude oil, the crude oil viscosity decreases significantly and the oil flow ability is improved to achieve the purpose of mixed-phase oil drive.

Under certain temperature and pressure conditions, when the crude oil is miscible with  $CO<sub>2</sub>$ , the interfacial tension of the crude oil is eliminated, and the pressure at this point is the minimum miscible pressure (MMP) for  $CO<sub>2</sub>$  miscible flooding. Therefore, understanding the interfacial properties of processes, such as the dissolution of  $CO<sub>2</sub>$  into crude oil, is particularly important for  $CO<sub>2</sub>$  miscible flooding technology. The MMP is the minimum pressure at which the interfacial tension between oil and gas disappears. The most commonly used experiments for determining MMP are the fine tube test method, the bubbler method, and the vanishing interfacial tension method.

The fine tube experiments is a standard method widely used and accepted in the petroleum industry to measure MMP and usually the measured MMP is reliable (Elsharkaw1996; Flock and Nouar 1984). Yelling et al. (1980) used sand-filled long fine tubes to simulate the  $CO<sub>2</sub>$  repulsion process in real reservoirs to determine MMP, and investigated the effect of reservoir temperature and oil compositions on MMP. Nouar and Flock(1984) performed a parameter analysis of the MMP determination using a thin-tube test and suggested that increasing the length of the thin-tube could result in more accurate MMP values. However, the fine tube test is very expensive and time consuming (Zhang and Gu 2015). The bubble-lift method is an relative cheap and fast method for determining MMP. The movement of  $CO<sub>2</sub>$ bubbles in oil is observed through a high-pressure window, and the oil-gas miscible state is determined by the change in appearance of the bubbles as they move at different pressures. However, the method relies on human observations and is subjective (Elsharkaw 1996; Dong 2001). The vanishing interfacial tension method was used to determine the interfacial tension between the injected gas and oil at constant temperature and pressure, and the pressure at which the interfacial tension is zero is obtained by extrapolation, i.e. the MMP (Rao 1997; Rao and Lee 2002; 2003). Ayirala and Rao demonstrated that the MMP determined using the vanishing interfacial tension method was similar to that was determined by the fine tube experiment and the bubble lifter method. The experiment results clearly supported that the use of vanishing interfacial tension for the rapid and economical determination of MMP (Ayirala and Rao 2011).

Due to the complex composition of crude oil, there are too many influencing factors if the properties of the system composed of  $CO<sub>2</sub>$  and crude oil are studied directly in the  $CO<sub>2</sub>$  flooding process. Therefore, researchers generally take the major components of oil to represent crude oil, such as n-alkanes, cycloalkanes aromatic hydrocarbons, etc. Shaver et al. (2001) experimentally measured the phase fraction, phase density and interfacial tension of CO<sub>2</sub> and n-decane in the pressure range of  $1~13$ MPa at 344 K. Hsu et al.(1985) measured the oil composition, oil density, and interfacial tension of CO<sub>2</sub> and n-butane system at the temperature of 319K~378K until the pressure achieved the MMP. Spee and Schneider (1991) measured the change of oil composition with pressure in a  $CO<sub>2</sub>/dodec$  system and  $CO<sub>2</sub>/1,8$ -octanediol system at 393 K and 10~100 MPa.

In recent years, molecular simulations have been widely applied to study the  $CO<sub>2</sub>$  and crude oil systems. Makimura et al. (2012) investigated two characteristics of  $CO<sub>2</sub>$ -EOR based on molecular simulations, including interfacial properties and phase equilibrium. Neyt et al. (2011) used Gibbs Ensemble Monte Carlo and two-phase Monte Carlo to calculate the interfacial tension between  $CO<sub>2</sub>$  and water, the interfacial tension between  $CO<sub>2</sub>$  and n-butane system. The calculated results were in good agreement with the experiment results. Müller etal .(2009) used molecular dynamics to calculate the oil composition, oil density, interfacial tension and interfacial structure of n-hexane and n-decane system, CO<sub>2</sub> and n-decane system, and ethane and n-eicosane system. The simulation results agreed well with the experiments. De

Lara et al. (2012) used molecular dynamics to investigate the interfacial properties of brine/light oil,  $CO_2$ /light oil, N<sub>2</sub>/ light oil and CH<sub>4</sub>/light oil systems. They showed that the CO<sub>2</sub>/light oil system had the advantage of lower interfacial tension and enhancing diffusion of  $CO<sub>2</sub>$  in the oil phase. The diffusion coefficients of n-alkanes from methane to tetradecane in  $CO<sub>2</sub>$  at infinite dilution were calculated by Feng et al. (2013). The results obtained from the simulations were reliable.

Compared to experimental methods, molecular simulations can be used to calculate the interfacial tension between  $CO_2$  and crude oil, to reveal the interfacial properties of  $CO_2$  and oil, and to observe microscopic mixing processes. These are difficult or impossible to be observed and measured using experimental methods. In addition, molecular dynamics simulations can be used to predict the interfacial properties of  $CO<sub>2</sub>$  and oil with low cost and fast calculation time.

In this study, the molecular dynamics simulation method was proposed to study the miscibility characteristics of injected  $CO<sub>2</sub>$  and oil in a block of Yanchang Oilfield. The paper is structured as follows: Section 2 describes the proposed methodology in details, including force field and MMP calculation methods; Section 3 describes the model used for the molecular simulations; Section 4 presents the main results of the study.

# **Methodology**

**Force Field**. The potential energy function describing the forces interacting between atoms in a system is called the force field. Constructing an accurate potential energy function for a system is an important step in molecular dynamics calculations. In general, molecular force fields mainly include bond stretching potential energy, bond angle bending potential energy, dihedral angle distortion potential energy, and non-bonding potential energy. Non-bonding potential energy includes van der Waals potential energy and Coulomb electrostatic potential energy.

Force fields have been developed for each system and are basically suitable for molecular dynamics simulation studies in various fields. Different force fields include different atom types, so before selecting a force field one should first check the list of atom types for the force field and whether the force field covers the atom types in the simulated system.

The available  $CO<sub>2</sub>$  molecular force fields are mainly divided into a rigid force field containing the TraPPE force field, a semi-flexible force field with the EPM2 force field and a flexible force field with the ZHU force field (Potoff and Siepmann 2001; Harris and Yung 1995; Zhu 2009). The molecular force fields of n-alkanes can be divided into two categories: joint atomic force fields and all-atomic force fields. Joint atomic force fields are those that equate CH<sub>3</sub> and CH<sub>2</sub> of n-alkanes as one atom, such as OPLS-UA, TraPPE-UA and NERD (Jorgensen 1984; Martin and Siepmann 1998; Nath 1998). All-atomic force fields are those all atoms expressed in n-alkanes explicitly, such as OPLS-AA and CHARMM (Jorgensen 1996; Price 2001; Davis 2008).

The ZHU force field was proposed by Zhu et al. (2009), which can accurately predict the saturated gas-liquid phase density, critical point properties, while taking into account the molecular structure properties of supercritical  $CO<sub>2</sub>$ , and is therefore suitable for the simulation of systems containing supercritical CO2. The calculated gas-liquid equilibrium curves from the NERD force field are in good agreement with experimental data for both shorter chain alkanes and longer chain alkanes (Müller 2009; Nath 1998). Therefore, the ZHU  $CO<sub>2</sub>$  force field and the NERD n-alkane force field were used in this study. The NERD molecular force field defines the total potential energy function of an alkane as shown in **Eq. 1**.

$$
V_{\text{total}} = \sum_{\text{bonds}} \frac{k_{ij}^b}{2} (r_{ij} - b_{ij})^2 + \sum_{\text{angles}} \frac{k_{ijk}^{\theta}}{2} (\theta_{ijk} - \theta_{ijk})^2 + \sum_{\text{dihedrals}} V_0 + V_1 (1 + \cos \psi) + V_2 [1 - \cos (2\psi)] + V_3 [1 + \cos (3\psi)] + \sum_{\text{nonbonded}} 4\varepsilon_{ij} \left[ \left(\frac{\sigma_{ij}}{r_{ij}}\right)^{12} - \left(\frac{\sigma_{ij}}{r_{ij}}\right)^{6} \right] + \frac{q_i q_j}{4\pi\varepsilon_0 \varepsilon_r r_{ij}} \dots \dots \dots \dots \dots \dots \dots \dots \dots \tag{1}
$$

The ZHU  $CO<sub>2</sub>$  force field function takes the form shown in Eq. 2.

total <sup>=</sup> bonds <sup>2</sup> − 2 <sup>+</sup> 2 − <sup>0</sup> 2 <sup>+</sup> 4 12 − 6 + 40,...(2)

Van der Waals interactions between atoms describe the interactions between atoms that are caused by non-covalent and non-hydrostatic forces that attract or repel each other. The Lennard-Jones potential function is a function that describes the Van der Waals interactions between atoms and has the form shown in **Eq. 3**.

$$
V_{LJ}(r_{ij}) = 4\varepsilon_{ij} \left[ \left( \frac{\sigma_{ij}}{r_{ij}} \right)^{12} - \left( \frac{\sigma_{ij}}{r_{ij}} \right)^{6} \right] \dots
$$

The sums between the different atoms are obtained by means of a mixing rule, the common Lorentz-Berthelot mixing rule, as shown in **Eq. 4 and 5**, respectively.

$$
\sigma_{ij} = \frac{\sigma_i + \sigma_j}{2}
$$
\n
$$
\varepsilon_{ij} = \sqrt{\varepsilon_i \varepsilon_j}
$$
\n(4)

**Simulation method**. In this study, Lammps molecular simulation software was used for the simulations. During the molecular dynamics (MD) simulations, periodic boundary conditions were used, the equations of motion were solved for integration using the Velocity-verlet method. The long-range force electrostatic interactions used the particle-particle-particle-mesh (PPPM) summation method with an accuracy of  $1.0 \times 10^{-4}$ . The non-bonded van der Waals forces used the 12-6 Lennar-Jones potential function with a truncation radius of 2 nm and a time step of 1 fs. The temperature coupling was performed using the Nosé-Hoover algorithm. The entire simulation time was 10 ns of relaxation time, 30 ns of calculation time, with data collected at 0.1 ps intervals. Finally, the IFT of the system was calculated.

There are many ways to obtain the MMP, the most common ones are to calculate the number of  $CO<sub>2</sub>$ and alkanes that cross the phase interface at the same temperature and different pressures as a percentage of the total number of CO<sub>2</sub> and alkanes, and to obtain the MMP when the number of ratios drops to a stable pressure. There are also methods to obtain the MMP by the disappearance of interfacial tension.

In this study, the MMP was obtained by the disappearance of interfacial tension, as the method has a clear definition of parameters. When the interfacial tension is zero, the interface between the two phases disappears, then the two phases can completely become a miscible phase. The Gibbs interfacial tension equation was used to calculate the variation of the two-phase interfacial tension with pressure, from which MMP is indirectly calculated. The specific expression is given as **Eq. 6**.

 = 1 2 0 <sup>−</sup> <sup>=</sup> 1 2 − + 2 ,..(6)

where  $\gamma$  is the interfacial tension, and  $P_N(z)$  and  $P_T(z)$  represents the normal and tangential pressures,  $P_{\alpha\alpha}$  is the amount on the diagonal of the pressure tensor, and  $L_z$  is the length in the z-direction of the simulated system.

**Modeling**. The force field parameters for this study are shown in **Table 1**. The initial systems of two cases are given in **Figure 1**, with a oil (liquid phase) in the middle and CO<sub>2</sub> (gas phase) in the two side. The oil phase consists of alkanes of different chain lengths, depending on the case. For the  $CO_2/n$ -decane system, the oil contains 800 n-decane molecules. The system pressure was varied with the number of  $CO<sub>2</sub>$ molecules in the gas phase on both sides. The size of the simulated system was taken to be  $5 \times 5 \times 30$  nm<sup>3</sup>. .

Atom		$\sigma(nm)$	$\varepsilon_{ij}$ (KJ/mol)		
$CT_CH_3$		0.3910	0.8647		
$CT_CH_2$		0.3930	0.3808		
$\mathbf C$		0.2800	0.23397		
$\Omega$		0.3028	0.66824		
Bond	$r_0(nm)$		$k_b(kJ/(mol/nm^2))$		
$CH_3$ $CH_2$	0.1540		80235.0280		
$CH2$ $CH2$	0.1540		80235.0280		
$C-O$	0.1162		60000.0000		
Angle	$\theta_0(\text{deg})$		$K_{\theta}$ (kJ/mol/rad <sup>2</sup> )		
$CH_3$ $CH_2$ -CH <sub>2</sub>	114		519.657		
$CH2$ $CH2$ $CH2$	114		519.657		
$C-O-C$	180		110.000		
Torsion	$V_0$ (kJ/mol)	$V_1$ (kJ/mol)	$V_2$ (kJ/mol)	$V_3$ (kJ/mol)	
$CH3$ $CH2$ $CH2$ $CH2$ $CH2$	0.0000	5.9038	$-1.1339$	13.1590	
$CH2 CH2 – CH2 – CH2$	0.0000	5.9038	$-1.1339$	13.1590	

**Table 1**—**Force field parameters.**



(a) Case 1



(b) Case 2 **Figure 1**—**Initial structure of the two systems.**

#### **Results and Discussion**

**Interfacial Tension and MMP**. The disappearance of interfacial tension method was used in the MD simulation to indirectly calculate the MMP of  $CO<sub>2</sub>$  with n-decane at 334K. Because Shaver (2001) experimentally measured the phase fraction, phase density and interfacial tension of  $CO<sub>2</sub>$  and n-decane in the pressure range of 1~13MPa at 344 K, the simulation results in this section are compared with the experimental values. As shown in **Figure 2(a)**, the calculated IFTs by this work were in very good agreement with Shaver (2001) method. The interfacial tension decreases with increasing pressure and displays a linear relationship, which indicates that the interface between  $CO<sub>2</sub>$  and alkane becomes increasingly blurred and gradually tends to a miscible phase. In addition, the linear relationship enables a reliable extrapolation to obtain the pressure when the interfacial tension is zero. Thus, the MMP was determined to be 11.89 MPa when IFT equal 0. The estimated MMP is very close to that measured MMP (12.74 MPa) by Shaver et al (2001).

As can be seen from **Figure 2(b)**, the relationship between interfacial tensions and pressure obtained by Müller and Mejía (2009) using the EPM2  $CO<sub>2</sub>$  model and the NERD n-decane model were in good agreement with the experiments. Mejia et al. (2014) used coarse-grained molecular model to simulate CO2/n-decane system. But the estimated interfacial tensions were slightly higher than the measured values. The estimated IFTs by this work agreed well with the measured values. Therefore, ZHU  $CO<sub>2</sub>$ model and the NERD n-alkane model used in this paper are an effective, convenient and low-cost method for predicting the MMP for  $CO<sub>2</sub>$  and alkane systems compared to coarse-grained simulations.



**Figure 2**—**Interfacial tension between carbon dioxide and n-decane with pressure.**

To validate the effectiveness of the proposed method in estimating MMP, the proposed method was compared to the empirical formulas. The comparison results are shown in **Table 2**. The National Petroleum Council (NPC) empirical equation estimates MMP roughly, mainly by using API and temperature as parameters, and obtains results with large errors. Yellig and Metcalfe (1980) proposed a method to predict MMP according to the temperature, which is one of the most common methods. The temperature is the only parameter in the formula:

=1833.7217+2.2518055(T-460)+0.01800674(T-460) <sup>2</sup> − 103949.93 −460 ......................................(7)

As can be seen from Table 2, the results of the NPC empirical formula approach are poor. The molecular simulation used in this study has a higher prediction accuracy than the Yellig-Metcalfe model. It indicates that the empirical formula has certain limitations, such as the composition of different oil fields, the composition of the injected gas, and the range of working conditions. Thus, the results obtained by the empirical formulas are difficult to be generalized. In contrast, the working conditions of the molecular simulation method proposed in this study is easy to set, and the calculated values agree well with the experimental values, so it has a wider applications.

MMP from experiment (MPa)	<b>NPC</b>		Yellig-Metcalfe (1980)		This study	
	<b>MMP</b>	Error	<b>MMP</b>	Error	<b>MMP</b>	Error
12.74	(MPa)	$\frac{6}{2}$	(MPa)	$\frac{0}{0}$	(MPa)	$(\%)$
	10.69	2.05	13.78	1.04	11.89	0.85

**Table 2**—**Comparisons between the proposed method and the empirical formulas.**

**Phase Interface Properties**. The phase interface properties of  $CO<sub>2</sub>$  and n-decane systems, such as interfacial structure and interfacial thickness, are difficult or impossible to be measured by experiments. However, molecular dynamics has the advantage of being intuitive and convenient for this purpose. In this section, the mixing process, interfacial structure and interfacial thickness of the  $CO<sub>2</sub>$  and n-decane system at 344 K were investigated. The dynamic mixing process of the  $CO<sub>2</sub>/n$ -decane system at 344 K are shown in **Figure** 3. A small amount of decane molecules were extracted by  $CO_2$  and moved towards the  $CO<sub>2</sub>$  phase, and the phase interface gradually disappeared; a large number of  $CO<sub>2</sub>$  molecules formed clusters around the decane molecules, and the two gradually miscible, and finally the phase interface disappeared and reached the mixed-phase state after 40ns.



(c) 15ns



**Figure 3**—**CO2/n-decane mixed-phase microscopic processes.**

The variation of the gas-liquid phase density with pressure for the  $CO<sub>2</sub>$  and n-decane system at 344 K is shown in **Figure** 4. As the pressure of the system increases, the system in the liquid phase area gradually expands, the gas-liquid phase density also increases and the phase interface gradually becomes thicker.



**Figure 4**—**Variation of gas-liquid phase density with pressure of CO2/n-decane system.**

The density distribution of CO<sup>2</sup> and n-decane in the system at different pressures is shown in **Figure 5**. As the pressure of the system increases, the density of n-decane decreases and the density of  $CO<sub>2</sub>$ increases. Part of the  $CO<sub>2</sub>$  in the system gathered at the interface to form a  $CO<sub>2</sub>$  adsorption layer, and the adsorption layer gradually became thicker as the pressure increased, which surface more and more  $CO<sub>2</sub>$ gathered at the interface as the pressure increased.



**Figure** 5—**Density** distribution of components of CO<sub>2</sub>/n-decane system at different pressures.

Base on the above analytical simulations, a mixture of n-decane and n-hexane was used to replace the oil from the Yanchang field and the MMP was determined. The results are shown in **Figure 6**, which shows an MMP of 11.4 MPa at 344 K. And the effect of the oil components on the MMP can also be illustrated with Figure 6, which shows that the addition of n-hexane has a significant effect on the MMP of n-decane and CO2. The addition of n-hexane makes the MMP decrease, because the light hydrocarbon components can be extracted from oil phase by  $CO<sub>2</sub>$ , when  $CO<sub>2</sub>$  contacts with the oil, while the light components originally were dissolved in the oil. As a result, it makes  $CO<sub>2</sub>$  become hydrocarbon rich. The enriched CO<sup>2</sup> then contacts with the oil to further extract the light components. The process repeats until  $CO<sub>2</sub>$  extracts enough alkanes. In contrast, when n-hexane is dissolved in the oil to contain more light components, so  $CO<sub>2</sub>$  can be more easier to extract enough light hydrocarbons to accelerate enrichment and make  $CO<sub>2</sub>$  be more easy miscible with the oil.



**Figure 6**—**Effect of oil composition on MMPs.**

**The Effects of Temperature on MMP.** It has been proven by numerous experiments that reservoir temperature has a significant effect on MMP and it is an important variable affecting MMP (Zolghadr 2013). The variation of MMP with temperature for the CO<sub>2</sub>/n-decane system is shown in **Figure** 7. At a low pressure, IFT decreases with increasing temperature. But at a high pressure, IFT increases with increasing temperature and MMP increases with increasing temperature. This is because the density of CO<sub>2</sub> is controlled by temperature and pressure.

As can be seen in **Figure 8**, at a constant pressure, the density of  $CO<sub>2</sub>$  decreases with increasing temperature, leading to a decrease in the solubility of  $CO<sub>2</sub>$  and in the extraction ability of light hydrocarbons. Thus, to give  $CO<sub>2</sub>$  sufficient solubility to achieve a mixed phase, it is necessary to increase the density of  $CO<sub>2</sub>$  by increasing pressure, so the MMP increases with increasing temperature.



**Figure 7**—**Effect of temperature on MMPs.**



**Figure 8**—**The density distribution of CO2/n-decane at 4.5 MPa.**

# **Conclusions**

In this paper, we simulated the phase density and interfacial tension of the  $CO<sub>2</sub>$  and n-decane system at 334 K under different pressures using molecular dynamics methods, analyzed the interfacial characteristics of the system, and investigated the effect of the addition of hexane on the minimum miscibility pressure of the CO<sub>2</sub> and n-decane system, and the main conclusions are as follows.

- 1. The MMP of  $CO<sub>2</sub>$  with n-decane at 334 K was predicted to be 11.89 MPa using the molecular simulation method, which has the advantage of being less costly and more efficient than the experimental methods, and the prediction is more realistic and reliable than the theoretical equations.
- 2. The proposed molecular dynamics simulation displayed the mixing process of  $CO<sub>2</sub>/n$ -decane system. In the process,  $CO_2$  is dissolved into n-decane, while n-decane is continuously extracted by  $CO_2$ . The interface between  $CO<sub>2</sub>$  and n-decane gradually disappears and the interfacial tension gradually decreases, and finally reaches the miscible state.
- 3. As the pressure of the system increases, the thickness of the phase interface between  $CO<sub>2</sub>$  and n-decane increases, and the CO<sub>2</sub> adsorption layer on the interface also gradually becomes thicker, and the density of n-decane decreases with the increase of pressure, while the density of  $CO<sub>2</sub>$  is the opposite.
- 4. When a certain amount of hexane is dissolved to the system of  $CO<sub>2</sub>$  and n-decane, the MMP of the system decreases. At a low pressure, the IFT decreases with increasing temperature; while at a high pressure, both the IFT and MMP increases with increasing temperature.

# **Conflicts of Interest**

The author(s) declare that they have no conflicting interests.

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